

## Saddle Points of the Complementary Error Function

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**Abstract.** The first one hundred zeros of the derivative of the function  $w(z) = e^{-z^2} \operatorname{Erfc}(-iz)$  are given, together with an asymptotic formula for estimating the higher zeros.

1. In a previous paper by the present authors [1], the zeros of the function

$$(1) \quad w(z) = e^{-z^2} \operatorname{Erfc}(-iz)$$

were obtained. In this paper, the values of  $z = x + iy$  for which

$$(2) \quad dw/dz = 0$$

are given. These points represent singular points of the family of curves

$$(3) \quad \phi(x, y) \equiv |w| = \text{const}$$

in the  $x$ - $y$  plane since at such a point the direction  $dy/dx$  of these curves is undefined. As in the case of the zeros of  $w(z)$ , the saddle points lie in the lower half-plane and are symmetrically located with respect to the  $y$ -axis. For convenience, we introduce the function  $Y(\rho) = (\sqrt{\pi}/2)w(i\rho)$ , which satisfies the differential equation

$$(4) \quad dY/d\rho = 2\rho Y - 1.$$

Thus, at a saddle point,  $\rho = \rho_n$ ,

$$(5) \quad 2\rho_n Y(\rho_n) = 1.$$

With the aid of the differential equation (4), we can expand  $Y$  in the vicinity of a saddle point as a Taylor series, viz.,

$$(6) \quad Y = +\frac{1}{2\rho_n} + \frac{1}{2\rho_n} (\rho - \rho_n)^2 + \frac{1}{3}(\rho - \rho_n)^3 + \dots .$$

Hence

$$(7) \quad \frac{1}{Y} = 2\rho_n - 2\rho_n(\rho - \rho_n)^2 - \frac{4\rho_n^2}{3} (\rho - \rho_n)^3 + \dots .$$

Introducing the variable  $t = \rho - 1/2Y$ , this may be written

$$(8) \quad \begin{aligned} t &= (\rho - \rho_n) + \rho_n(\rho - \rho_n)^2 + \frac{2\rho_n^2}{3} (\rho - \rho_n)^3 + \dots \\ &= (\rho - \rho_n) + \rho(\rho - \rho_n)^2 - \left[ 1 - \frac{2\rho^2}{3} \right] (\rho - \rho_n)^3 + \dots . \end{aligned}$$

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Received June 26, 1972.

AMS (MOS) subject classifications (1970). Primary 33A20.

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Therefore

$$(9) \quad \rho - \rho_n = t - \rho t^2 + [1 - 8\rho^2/3]t^3 + \dots,$$

or

$$(10) \quad \rho_n = \rho - t + \rho t^2 - [1 - 8\rho^2/3]t^3 + \dots.$$

Equation (3) may also be expressed in terms of  $Y$  as follows:

$$(11) \quad \rho_n = \frac{1}{2Y} \left[ 1 + t^2 + \frac{4}{3Y} t^3 + \dots \right].$$

The above series will converge rapidly if  $\rho$  is close to a saddle point  $\rho_n$ . In the next section, an asymptotic approximation to the saddle points is derived which may be used as a first approximation. By computing the corresponding values of  $Y$  and  $t$  and substituting these into Eq. (11), an improved approximation to  $\rho_n$  is obtained. If necessary,\* the process may be repeated using the newly computed value of  $\rho$ , and continued until convergence is reached. A sample calculation leading to the first saddle point is given at the end of the next section.

**2. Asymptotic Approximation to the Saddle Points.** At a saddle point, we have, from Eq. (5),  $2\rho Y = 1$  or

$$(12) \quad w = +i/\pi^{1/2}z.$$

The saddle points are assumed to be of the form  $z = x - iy$ , with  $x > 0$ ,  $y > 0$ . Setting  $w(x + iy) = u + iv$ , Eq. (12) is equivalent to

$$(13) \quad 2e^{y^2-x^2}e^{2ixy} - u + iv = i/\pi^{1/2}z.$$

Replacing  $w$  by the first three terms of the continued fraction gives

$$(14) \quad u - iv = -\frac{i}{\pi^{1/2}} \left[ \frac{z^2 - 1}{z(z^2 - 3/2)} \right],$$

and Eq. (13) becomes

$$(15) \quad 2e^{y^2-x^2}e^{2ixy} \doteq \frac{-i}{\pi^{1/2}} \left\{ \frac{1}{z[2z^2 - 3]} \right\}.$$

Since  $\arg(z) = -\pi/4 + \sigma$ , it follows that the argument of the right side of (15) is  $\pi/4 - \sigma$ . Hence,

$$(16) \quad 2xy = (2n + \frac{1}{4})\pi + \beta,$$

where  $0 \leq \beta \leq \pi/2$  and since, asymptotically,  $x \doteq y$ , we take, as the limiting value of  $x$  and  $y$ ,

$$(17) \quad \lambda = ((n + \frac{1}{8})\pi)^{1/2}$$

and set\*\*

\* By computing a sufficient number of additional terms in Eq. (11), only one application would be required.

\*\* For the justification of this form, see [1, Eq. (29)].

$$(18) \quad x = \lambda + \alpha + p, \quad y = \lambda - \alpha + p.$$

From Eq. (16) we have, equating magnitudes,

$$(19) \quad 2e^{-4\lambda\alpha - 4\alpha p} \doteq \frac{1}{2\sqrt{\pi}(x^2 + y^2)^{3/2}} = \frac{1}{2^{5/2}\sqrt{\pi}[\lambda^2 + \alpha^2 + 2\lambda p]^{3/2}}$$

$$= \frac{1}{2^{5/2}\sqrt{\pi}\lambda^3[1 + 2p/\lambda + (\alpha/\lambda)^2]^{3/2}}.$$

Hence

$$(20) \quad 2e^{-4\lambda\alpha} = 1/2^{5/2}\pi^{1/2}\lambda^3;$$

$$(21) \quad \alpha \doteq \ln(128\pi\lambda^6)/8\lambda.$$

The value of  $p$  is determined by equating arguments in Eq. (15). We find, denoting the argument of the right side by  $\phi$ ,

$$(22) \quad \tan 2xy \doteq 1 + 4\alpha^2 - 8\lambda p;$$

$$(23) \quad \tan \phi \doteq 1 - 6\alpha/\lambda + 3/2\lambda^2.$$

This gives

$$(24) \quad p \doteq (8(\lambda\alpha)^2 - 12(\lambda\alpha) + 3)/16\lambda^3.$$

Thus, the desired asymptotic approximation to three terms is

$$(25) \quad \left\{ \begin{array}{l} x \\ -y \end{array} \right\} = \lambda \pm \frac{1}{8\lambda} \ln(128\pi\lambda^6) + \frac{\frac{1}{8}[\ln(128\pi\lambda^6)]^2 - \frac{3}{2} \ln(128\pi\lambda^6) + 3}{16\lambda^3}.$$

The use of the approximation (25) in conjunction with Eq. (11) is illustrated below for the first saddle point. Equation (17) with  $n = 1$  gives

$$(26) \quad \lambda = 1.8799712060$$

and this, when substituted into Eq. (25), gives

$$(27) \quad x \doteq 2.5332619139, \quad y \doteq -1.2321384069.$$

The corresponding value of  $Y$  is

$$(28) \quad Y = -.0766358650 + .1594090127i.$$

Thus

$$(29) \quad t = -.0073085147 + .0144867658i.$$

Substituting in Eq. (11) the values of  $t$  and  $y$  as given by Eqs. (28) and (29), we arrived at the improved values

$$(30) \quad x \doteq 2.5471305433, \quad y \doteq -1.2251557198,$$

the corresponding values of  $Y$  and  $t$  being

$$(31) \quad Y = -.07667898752 + .1594172691i$$

$$t = .00000137615 - .00000251508i.$$

Zeros of  $w'(z)$

N	X	Y	N	X	Y
1	2.5471286282E+J0	-1.2251570959E+00	51	1.2883628281E+01	-1.2464770926E+01
2	3.161939531E+00	-2.025961307E+00	52	1.3005504374E+01	-1.2589548699E+01
3	3.6599721638E+00	-2.6288721547E+00	53	1.3126239378E+01	-1.2713113798E+01
4	4.0833844384E+00	-3.1323514518E+00	54	1.3245864838E+01	-1.2839507012E+01
5	4.4663513869E+00	-3.5728492033E+00	55	1.3364410869E+01	-1.2956742377E+01
6	4.8165949556E+00	-3.9699173288E+00	56	1.3481906248E+01	-1.3076870288E+01
7	5.1415732873E+00	-4.3318395797E+00	57	1.3598378492E+01	-1.3199914484E+01
8	5.4461347735E+00	-4.6684220832E+00	58	1.3713853935E+01	-1.3313903689E+01
9	5.7337608049E+00	-4.9836711355E+00	59	1.3828357802E+01	-1.3430865384E+01
10	6.0070346327E+00	-5.2811402113E+00	60	1.3941914268E+01	-1.3546825878E+01
11	6.2679376653E+00	-5.5634993766E+00	61	1.4054546519E+01	-1.3661810379E+01
12	6.5180322553E+00	-5.8328143120E+00	62	1.4166276813E+01	-1.3775843054E+01
13	6.7585678528E+00	-6.0976721515E+00	63	1.4277126525E+01	-1.3888947939E+01
14	6.9905787939E+00	-6.3385432717E+00	64	1.4387116197E+01	-1.4001144760E+01
15	7.2149102067E+00	-6.5773658881E+00	65	1.4496265507E+01	-1.4112457444E+01
16	7.4323664525E+00	-6.8008945823E+00	66	1.4604593703E+01	-1.4222905709E+01
17	7.6433572151E+00	-7.0134930011E+00	67	1.4712118848E+01	-1.4332509334E+01
18	7.8485984629E+00	-7.2482123176E+00	68	1.4818858656E+01	-1.4441287357E+01
19	8.0484883808E+00	-7.4588130776E+00	69	1.4924830120E+01	-1.4549258111E+01
20	8.2434276772E+00	-7.6637818847E+00	70	1.5030049632E+01	-1.4656439265E+01
21	8.4337692264E+00	-7.8635443393E+00	71	1.5134533006E+01	-1.4762847849E+01
22	8.6198257218E+00	-8.0584752099E+00	72	1.5238295510E+01	-1.4868500294E+01
23	8.8018758200E+00	-8.2489065255E+00	73	1.5341351892E+01	-1.4973412456E+01
24	8.9801691250E+00	-8.4351340870E+00	74	1.5443716400E+01	-1.5077599645E+01
25	9.1549302694E+00	-8.6174227572E+00	75	1.5545402812E+01	-1.5181076652E+01
26	9.3263622857E+00	-8.7960130063E+00	76	1.5646424452E+01	-1.5283857772E+01
27	9.4946494133E+00	-8.9711134684E+00	77	1.5746794214E+01	-1.5385956882E+01
28	9.6599594522E+00	-9.1429259916E+00	78	1.5846524580E+01	-1.5487387190E+01
29	9.8224457500E+00	-9.3116260862E+00	79	1.5945627637E+01	-1.5588161800E+01
30	9.9822488903E+00	-9.4773760740E+00	80	1.6044115098E+01	-1.5688293186E+01
31	1.0139498135E+01	-9.643246831E+00	81	1.6141998312E+01	-1.5787793485E+01
32	1.0294312663E+01	-9.8006685869E+00	82	1.6239288287E+01	-1.5886674456E+01
33	1.0446862641E+01	-9.9583537267E+00	83	1.6335995699E+01	-1.5984947497E+01
34	1.0597070153E+01	-1.0113676453E+01	84	1.6432136905E+01	-1.6082623664E+01
35	1.0745209996E+01	-1.0266684513E+01	85	1.6527703961E+01	-1.6179713679E+01
36	1.0891310412E+01	-1.0417477933E+01	86	1.6622724632E+01	-1.6276227949E+01
37	1.1035453688E+01	-1.0566149750E+01	87	1.6717202401E+01	-1.6372176576E+01
38	1.1177716709E+01	-1.0712786621E+01	88	1.6811146485E+01	-1.6467569372E+01
39	1.1318171446E+01	-1.0857469582E+01	89	1.6904565840E+01	-1.6562415867E+01
40	1.1456885382E+01	-1.1000274370E+01	90	1.6997469177E+01	-1.6656725323E+01
41	1.1593921898E+01	-1.1141271981E+01	91	1.7089864966E+01	-1.6750506743E+01
42	1.1729340610E+01	-1.1280529058E+01	92	1.7181761443E+01	-1.6843758883E+01
43	1.1863197640E+01	-1.1418108258E+01	93	1.7273166646E+01	-1.6936520258E+01
44	1.1995546087E+01	-1.1554068572E+01	94	1.7364088366E+01	-1.7028769153E+01
45	1.2126435874E+01	-1.1688465623E+01	95	1.7454534212E+01	-1.7120523634E+01
46	1.2255914076E+01	-1.1821351925E+01	96	1.7544511589E+01	-1.7211791552E+01
47	1.2384025412E+01	-1.1952777125E+01	97	1.7634027714E+01	-1.7302580552E+01
48	1.2510814479E+01	-1.2082748211E+01	98	1.7723089617E+01	-1.7392898083E+01
49	1.2636318910E+01	-1.2211429714E+01	99	1.7811704155E+01	-1.7482751401E+01
50	1.2760578027E+01	-1.2338743879E+01	100	1.7899878011E+01	-1.7572147579E+01

This leads to the next approximation

$$(32) \quad x \doteq 2.5471280282, \quad y \doteq -1.2251570959.$$

which is now correct to eleven figures, the error being  $O(t^4)$ .

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1. HENRY E. FETTIS, JAMES C. CASLIN & KENNETH R. CRAMER, "Complex zeros of the error function and of the complementary error function," *Math. Comp.*, v. 27, 1973, pp. 401-407.